

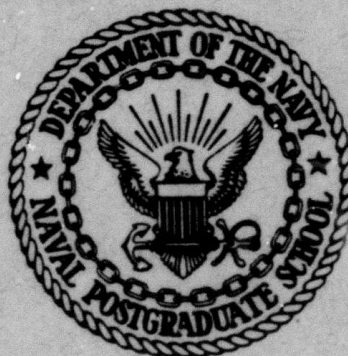
2

001CR
NPS67-82-003CR

AD A118241

NAVAL POSTGRADUATE SCHOOL

Monterey, California



DTIC
ELECTE
AUG 16 1982
H

SOLID BODY EQUATIONS TO CALCULATE THE
TRAJECTORY OF RAMJET

KENJI IMAI
NATIONAL DEFENSE ACADEMY
2-12-34 FUJIMICHO
HIGASHIMURAYAMA-CITY
TOKYO 189 JAPAN

APRIL 1982

Approved for public release; distribution unlimited

Prepared for:
Naval Postgraduate School
Monterey, California 93940

82 08 16 160

DTIC FILE COPY

NAVAL POSTGRADUATE SCHOOL
Monterey, California

Rear Admiral J. J. Ekelund
Superintendent

D. A. Schrady
Acting Provost

The work presented in this report is in support of solid fuel ramjet research sponsored by Defense Advanced Research Projects Agency (DARPA). Another goal of the research is to explore Navy Applications for Advanced Indirect Fire Support, AIFS: The AIFS project is also funded by DARPA.

The work reported herein was carried out for the Naval Postgraduate School by Dr. K. Imai, National Defense Academy under contract number 82-M-1221. The work was part of a program entitled Application of AIFS Technology to Navy Missions funded in part by DARPA and under the cognizance of Distinguished Professor A. E. Fuhs.

This report was prepared by:

Kenji Imai

DR. KENJI IMAI
2-12-34 Fujimicho
Higashimurayama-City
Tokyo 189 Japan

Publication of the report does not constitute approval of the sponsor for the findings or conclusions. It is published for information and for the exchange and stimulation of ideas.

Reviewed by:

Allen E. Fuhs

ALLEN E. FUHS
Distinguished Professor

Daniel J. Collins

DANIEL J. COLLINS, ACTING CHAIRMAN
Department of Aeronautics

Released by:

William M. Tolles

W. M. TOLLES
Dean of Research

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

RMS REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NPS67-82-003CR-001CR	2. GOVT ACCESSION NO. AD-A118241	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) SOLID BODY EQUATIONS TO CALCULATE THE TRAJECTORY OF RAMJET	5. TYPE OF REPORT & PERIOD COVERED CONTRACTOR REPORT April 1982	
	6. PERFORMING ORG. REPORT NUMBER	
7. AUTHOR(s) Kenji Imai	8. CONTRACT OR GRANT NUMBER(s) N62271-82-M-1221	
9. PERFORMING ORGANIZATION NAME AND ADDRESS NATIONAL DEFENSE ACADEMY 2-12-34 FUJIMICHO, HIGASHIMURAYAMA-CITY TOKYO 189 JAPAN	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS DARPA ORDER 4035 Element: 62702E	
11. CONTROLLING OFFICE NAME AND ADDRESS LCOL RENE LARRIVA, USMC DEFENSE ADVANCED RESEARCH PROJECTS AGENCY 1400 WILSON BLVD., ARLINGTON, VA 22209	12. REPORT DATE April 1982	
	13. NUMBER OF PAGES 19	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) NAVAL POSTGRADUATE SCHOOL MONTEREY, CA 93940	15. SECURITY CLASS. (of this report) UNCLASSIFIED	
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report) Approved for Public Release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES Principal investigator, Dr. Allen E. Fuhs, Distinguished Professor Department of Aeronautics, Naval Postgraduate School, Monterey, California 93940		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Six-degree-of-freedom trajectory ramjet projectile, exterior ballistics, gun launched ramjet, ramjets		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Six-degree-of-freedom trajectory equations for a ramjet propelled, gun launched projectile are formulated. An outline for FORTRAN computer program flow charts also appear in the report. Special emphasis is given to the effect of wind on trajectory errors.		

DTIC
SELECTED
AUG 16 1982
H

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 66 IS OBSOLETE
S/N 0102-LP-014-6601UNCLASSIFIED
SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

TABLE OF CONTENTS

	PAGE
ABSTRACT	
NOTATION	v
1. Introduction	1
2. Coordinate Systems	2
3. Trajectory Equations	4
4. Effect of Wind	5
5. Effect of Canard	6
6. Program Flow Charts	7
7. Conclusions	16
8. Acknowledgment	16
References	17

Accession For	
NTIS GRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By _____	
Distribution/	
Availability Codes	
Dist	Avail and/or Special
A	



Notation

C_D	: Drag Coefficient
$C_{L\alpha}$: Lift differential coefficient
$C_{m\alpha}$: Static moment differential coefficient
C_ϵ	: Resultant force of perturbing influences
d	: Diameter
F	: Force
g	: Acceleration of gravity
I	: Moment of inertia around lateral axis of projectile
I_x	: Moment of inertia around longitudinal axis of projectile
m	: Mass
M	: Moment
M_ϵ	: Resultant moment of perturbing influences
p	: Angular velocity around x_B axis
q	: Angular velocity around y_B axis
r	: Angular velocity around z_B axis
r_t	: Distance between center of gravity and nozzle throat
v	: Velocity
w	: Wind velocity
x, y, z	: Ground axis coordinates
α	: Angle of attack
β	: Side slip angle
θ, δ	: Angles defined in Chapt. 3 (2)
ϕ, ϵ	: Angles defined in Chapt. 3 (3)
η	: Angle rotated around x_B axis

μ : Factor angle of trim of canard
 v : Trim angle of canard
 π : Factor angle caused by attitude of projectile
 ρ : Density of air

Suffix :

a : Wind axis coordinate
 b : Body axis coordinate
 v : Velocity axis coordinate
 x,y,z : Rectangular axis

1. INTRODUCTION

Solid body equations to calculate the trajectory of a projectile which is flying with thrust of ramjet under hypersonic Mach number are formulated. The projectile is gun launched. This projectile has an axisymmetric configuration and is fin stabilized with four pop-out wings. The projectile has canards to control attitude. Ideally the projectile has no spin; however, due to effects from miscellaneous forces and moments which work on the body, it may acquire spin motion.

In order to calculate the trajectory considering such conditions, solid body equations with 6 degrees of freedom are induced. One of the main problems which will occur during flight motion of the projectile is trajectory errors which are caused by numerous origins especially due to the wind.

Total range of these projectiles are rather great. Consequently, perturbing influences from these origins are important to notice when long range trajectories are calculated. Some of the primary origins of error are mass unbalance due to impreciseness of construction and from shock of launching, misalignment of jet, misalignment of intake air flow, and so on. (1)

In order to minimize these effects, it is useful to set the value of thrust of the ramjet equal and opposite to that of aerodynamic drag. The trajectory is equivalent to projectile flight in a vacuum and is known as thrust-equal-drag trajectory. The effect of wind, when the direction of wind is the same as that of the trajectory, can be readily calculated. In case of a side wind, the projectile will be carried laterally.

In order to cancel the effect of a side wind which will carry the projectile laterally and to restore the planar motion of the trajectory, active control can be used. For example, canards can be employed. Due to active aerodynamic control, total range will be affected. Active control modulates aerodynamic drag. The boundary and initial conditions will influence whether total range will be expanded or shortened by the effect of canards.

In this paper, effects due to winds are considered; however, perturbations of other origins are concentrated in one term in the equations of motion as constants. In order to calculate these data by electronic computer, flow diagrams for FORTRAN are indicated.

2. Coordinate Systems

In order to construct solid body equations, coordinate systems are considered as follows: ⁽²⁾

(1) Ground axis coordinate system (0-xyz).

The origin is on the center of gravity of the projectile at the time of departure of projectile. The x axis is toward the direction of horizontal line of shot. The y axis is vertically upright, and the z axis is horizontally rectangular in a right hand sense.

(2) Velocity axis coordinate system (0- $x_v y_v z_v$).

The origin is at the center of gravity, CG, of the projectile.

The x_v axis is along the velocity vector of the projectile, i.e., x_v is tangent to the trajectory. The transformation to create the (x_v, y_v, z_v) coordinate system from the (x, y, z) coordinate system is, first, a rotation about the z axis by an angle θ .

A new coordinate system is formed and is identified as the (x_1, y_1, z) coordinate system.

The velocity vector, \vec{v} and x_v are located in the x_1 - z plane.

Now rotate the (x_1, y_1, z) coordinate system about the y_1 axis until the x_1 axis is parallel with \vec{v} . The angle of rotation about the y_1 axis is σ . The resulting coordinate system is the (x_v, y_v, z_v) system. Refer to Figure 1 for an illustration of the axes.

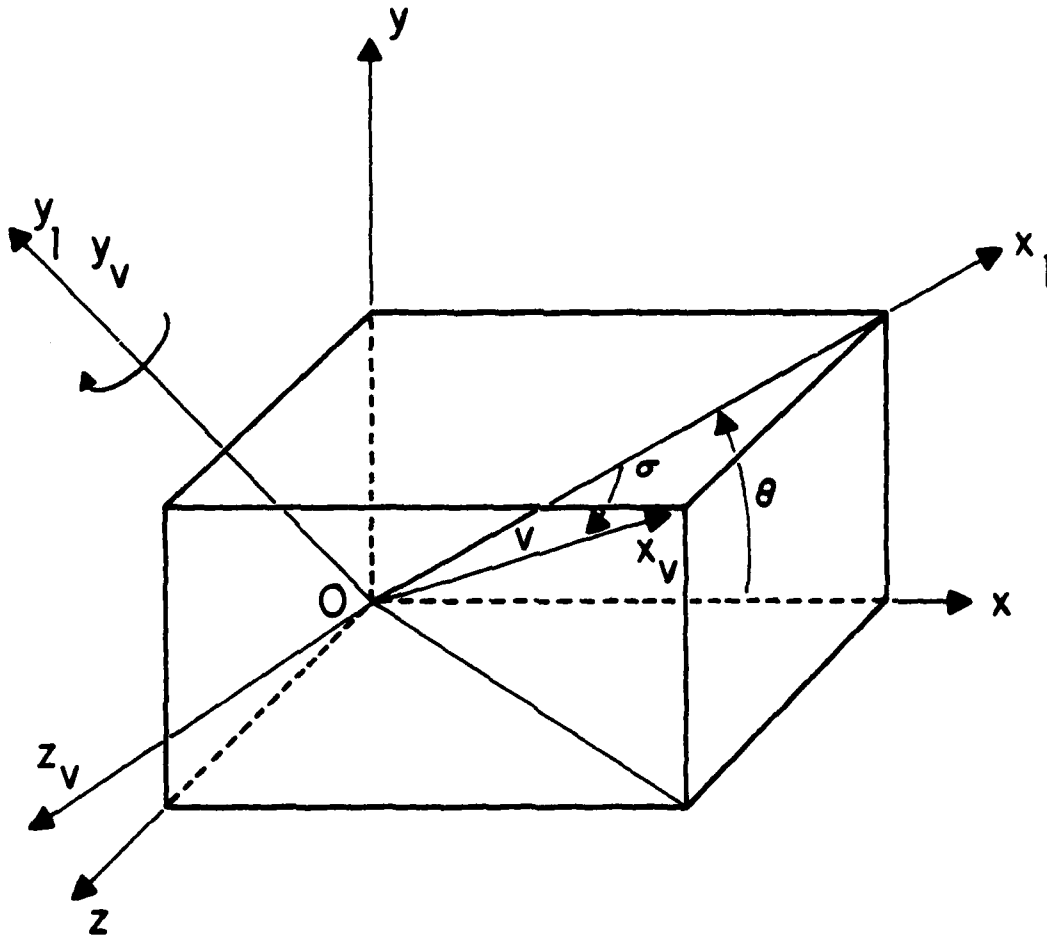


Figure 1. Illustration of geometry for the velocity axis coordinate system.

- (3) Nonrotating body axis coordinate system ($0 - x_B y_B z_B$).

The origin is at the center of gravity of projectile: the x_B axis coincides with the longitudinal axis of symmetry. The y_B and z_B axis are transformed in the same manner as that of velocity axis coordinate system by ϕ instead of θ , and by ξ instead of σ .

- (4) Wind axis coordinate system ($0 - x_{va} y_{va} z_{va}$). The system moves with relative wind speed similar to velocity axis coordinate system. The relevant angles are (θ_a, σ_a) instead of (θ, σ) with the x_{va} axis along the relative velocity vector.

3. Equations

Solid body equations with six degrees of freedom are developed by the method of coordinate transformation in order to calculate the trajectory of the projectile with ramjet propulsion as follows:

$$\dot{x} = v \cos \theta \cos \sigma \quad (1)$$

$$\dot{y} = v \sin \theta \cos \sigma \quad (2)$$

$$\dot{z} = -v \sin \sigma \quad (3)$$

$$\dot{v} = \frac{1}{m} F_{xv} \quad (4)$$

$$\dot{\theta} = \frac{1}{mv \cos \sigma} F_{yv} \quad (5)$$

$$\dot{\sigma} = -\frac{1}{mv} F_{zv} \quad (6)$$

$$\dot{\phi} = r / \cos \xi \quad (7)$$

$$\dot{\xi} = q \quad (8)$$

$$\dot{\eta} = r \tan \xi \quad (9)$$

$$\dot{b} = M_{xB}/I_x \quad (10)$$

$$\dot{q} = (1 - I_x/I)pr + M_{yB}/I \quad (11)$$

$$\dot{r} = -(1 - I_x/I)pq + M_{zB}/I \quad (12)$$

$$F_{xv} = -mg \sin \theta \cos \sigma + T \cos (\varphi - \theta) - \frac{1}{2} \rho v^2 S C_D \quad (13)$$

$$F_{yv} = -mg \cos \theta - T \alpha + \frac{1}{2} \rho v^2 S C_{L_\alpha} \alpha + C_E \cos \pi \quad (14)$$

$$F_{zv} = -mg \sin \theta \sin \sigma - T \beta + \frac{1}{2} \rho v^2 S C_{L_\alpha} \beta + C_E \sin \pi \quad (15)$$

$$M_{xB} = 0 \quad (16)$$

$$M_{yB} = \frac{1}{2} \rho v^2 S d C_{m_\alpha} \beta - Tr_t \beta + M_E \cos \pi \quad (17)$$

$$M_{zB} = \frac{1}{2} \rho v^2 S d C_{m_\alpha} \alpha - Tr_t \alpha + M_E \sin \pi \quad (18)$$

$$\alpha = \tan^{-1} \frac{\cos \xi \sin(\varphi - \theta)}{\cos \sigma \cos \xi \cos(\varphi - \theta) + \sin \sigma \sin \xi} \quad (19)$$

$$\beta = \tan^{-1} \frac{\sin \sigma \cos \xi \cos(\varphi - \theta) - \cos \sigma \sin \xi}{\cos \sigma \cos \xi \cos(\varphi - \theta) + \sin \sigma \sin \xi} \quad (20)$$

For a projectile with ramjet propulsion, eq. (16) is true usually. At launch, $\dot{p} = 0$, and there is no initial spin so that $p = 0$. For case of $p = 0$, equations (11) and (12) become

$$\dot{q} = M_{yB}/I \quad (11)'$$

$$\dot{r} = M_{zB}/I \quad (12)'$$

Furthermore, if thrust has a value near to drag, then dispersion becomes a minimum so that the last terms of equations (14), (15), (17) and (18) are deleted from these equations.

Effect of Wind

When a wind blows, a wind axis coordinate system is considered. Using these coordinates, the x axis is along the relative velocity between projectile and air. The motion of the projectile can be calculated the same way as in the case of no wind. For this case, we use a subscript (a) which is applied to the notations of the case of no wind.

In order to obtain velocities which were observed from the ground, we must add distances transported by wind during the time interval to values calculated on the wind axis coordinate. The relations between velocities on wind axis coordinate and velocity axis coordinate are as

$$\begin{cases} v_a \cos \theta_a \cos \sigma_a = v \cos \theta \cos \sigma - w_x & (21) \\ v_a \sin \theta_a \cos \sigma_a = v \sin \theta \cos \sigma - w_y & (22) \\ v_a \sin \gamma_a = v \sin \sigma + w_z & (23) \end{cases}$$

From these equations, we can calculate v_a , θ_a , σ_a knowing data without wind, v , θ , σ and the component of wind relative to the ground $w_x w_y w_z$.

In the case of computer calculation by a step-by-step method we can use (21), (22), (23) to get initial value of v , θ , σ in each successive step. These values of v , θ , σ are relative to the ground axis coordinates, so that the trajectory is obtained from them.

4. Effect of Canard

From mentioned above, it is clear that projectile is not within the plane of launching but flies in a different direction from the first schedule when wind is blowing. In order to cancel the miss distance, we can use a canard giving some suitable trim angle. Trim angle will be given on body axis coordinate and whose effect will act as sinusoidal form such as $v \sin \mu$ where μ is factor angle measured from y_B axis right wise around x_B axis. In order to cancel the effect of sidewise dispersion $\dot{z} = 0$ so $\sigma = 0$, $\sigma_a = 0$ must be satisfied.

therefore

$$F_{zv} = 0 \quad (24)$$

In order to demand (24) we must add a term for the canard on the right terms of eq. (15)

$$-mg \sin \theta \sin \sigma - T\beta + \frac{1}{2} \rho v^2 S C_{L_\alpha} \beta + C_e \sin \pi = v \sin \mu \quad (25)$$

There are many factors to give effect to the left side terms of this equation, so it is difficult to discuss analytically. However, the value of the terms are calculated on each step so that we can decide a suitable value of canard angle for each step of the calculation.

5. Program Flowcharts

In order to calculate these equations, a computer program will be built.⁽³⁾ It is illustrated by program flowcharts. This computer program consists of a main program and subroutines.

Inputs which are used for calculation are ready and stored in increment address by orders in the program to use for calculation. Data calculated are provided printed on sheets and so on. Program flowcharts of main program and subroutines are shown on figures, and they are explained as follows:

a. Main Program

Main program has a job to store and supply data from increment address of computer and to make initial condition in shape suitable for calculation. It gives these data of subroutines to compute and to get results of calculation. Data returned from subroutine are printed periodically. Calculation is carried by one step of variables.

These data are accumulated step-by-step until they come to some objective point. When the objective point is satisfied, the calculation is stopped. The point where the projectile touched the ground, point of print and points to change initial conditions are detected and ordered to computer. It contains FORMAT to print these results.

b. Subroutine COMPUTE

In order to calculate eq. (1) ~ (12) there need data of eq. (13) ~ (20) which are in the state suitable for input. In this subroutine these data are prepared using three subroutines of ATOM, FORCE and MOMEN. These data are sent to subroutine RKG. There eq. (1) ~ (12)

are calculated and results are sent back to this routine. Additional data are calculated here. These data are sent back to main program.

t. Subroutine RKG

This subroutine has a job to calculate each of the differential equations in a Runge-Kutta-Gill method. Suitable data for input are sent from subroutine COMPUTE. This subroutine calls differential equations one by one from subroutine DANDO.

d. Subroutine DANDO

This subroutine stores each equations whwch composes the trajectory equations in state of FORTRAN form.

e. ATOM

This subroutine provides air temperature and air density for the standard state of heights from sea level. Air temperature is used to calculate Mach number.

f. FORCE

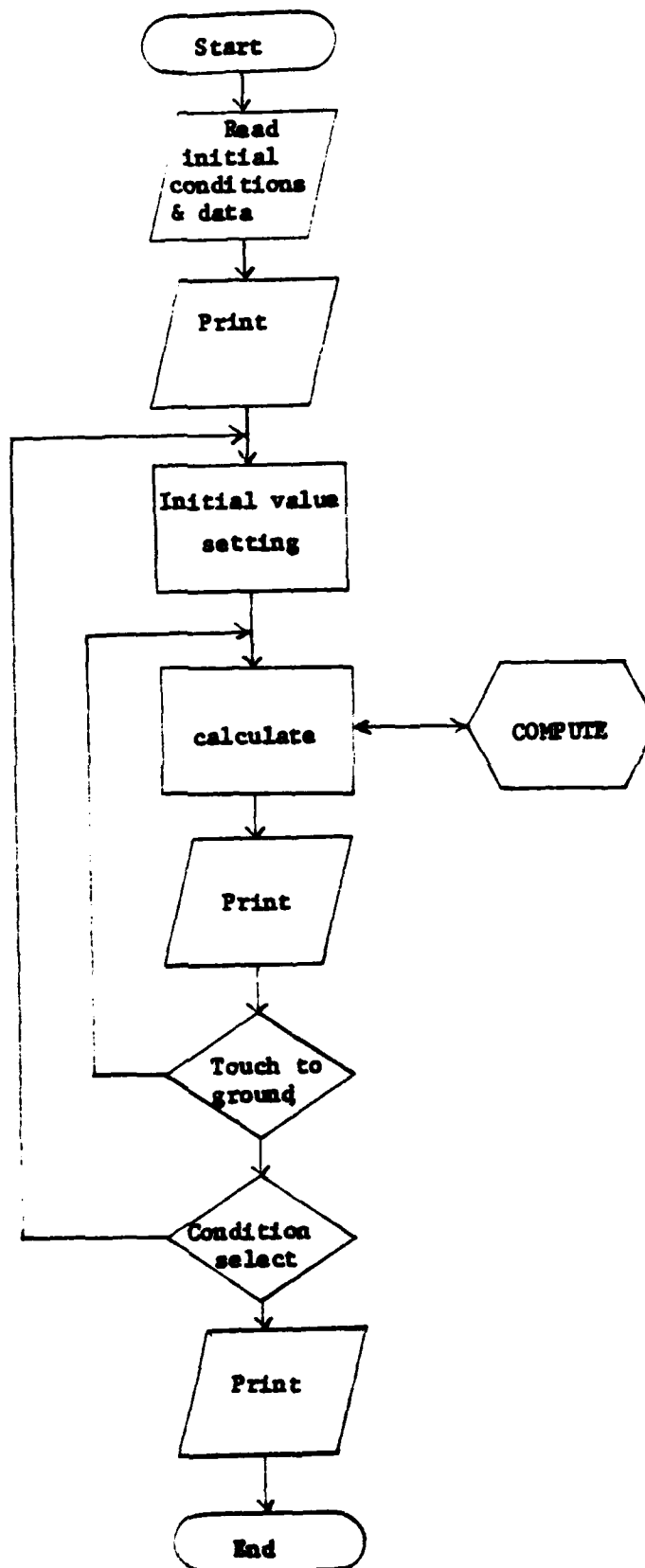
Data of forces are stored in increment address. On this subroutine forces that are arranged suitably to the state of input of the instance are selected and prepared for supply. This subroutine has a function to make linear interpolation.

g. MOMEN

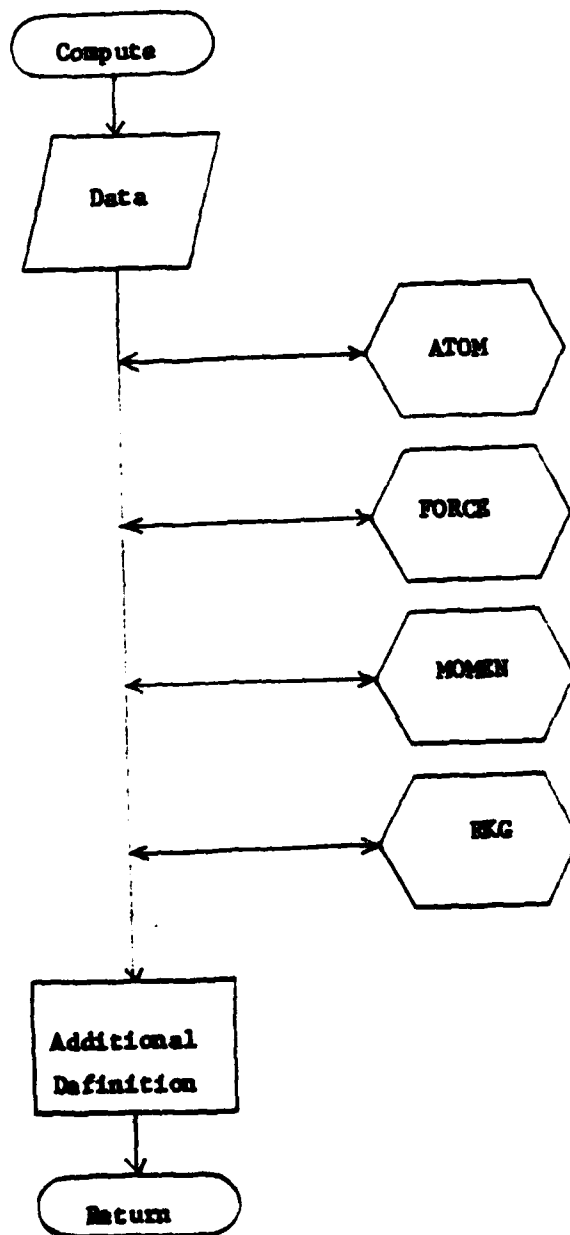
Data of moments are stored in increment address. Moments that are arranged suitably to the state of input of the instance are selected and prepared to supply. This subroutine has a function to make linear interpolation.

Program Flow Charts

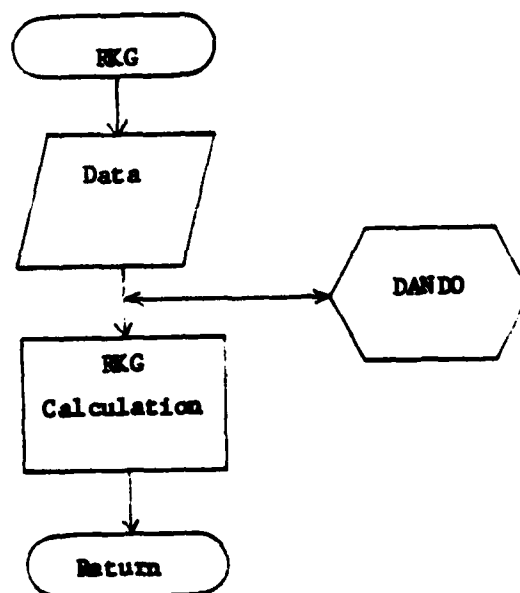
(a) Main Program



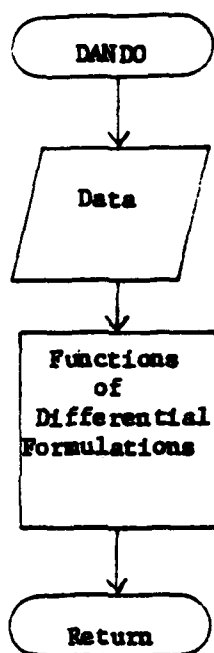
(b) Subroutine COMPUTE



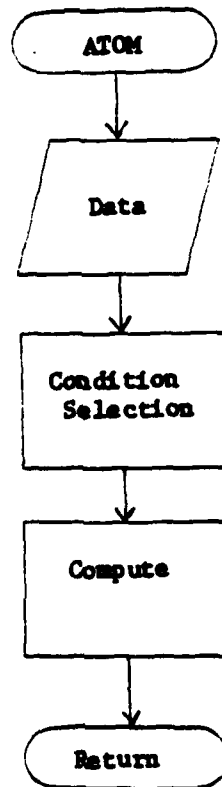
(C) Subroutine HKG



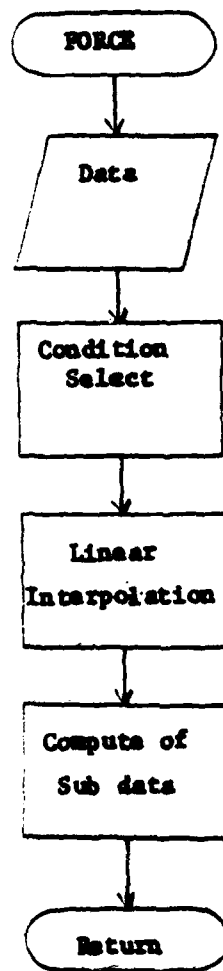
(d) Subroutine DANDO



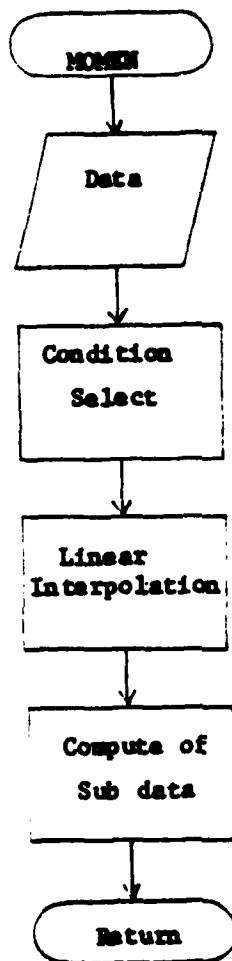
(e) Subroutine ATOM



(f) Subroutine FORCE



(g) Subroutine MOMEN



6. Conclusions

Solid body equations with 6-degree-of-freedom are formulated in order to calculate the trajectory of a projectile which is flying with the thrust of a ramjet.

In order to calculate by electronic digital computer; program flow charts are developed. FORTRAN programs will be made for each subroutine and program. Trajectory errors due to the effect of the wind are considered mainly. Dispersion due to the wind will be calculated by these programs. If there need to cancel the effect of a side wind, trim angle of canard will be given step by step in the procedure of calculation.

7. Acknowledgment

This research was sponsored by DARPA. The author wishes to express his deep thanks to Distinguished Professor Allen E. Fuhs for his help.

References:

1. Gantmakher, F. R., "The Flight of Unguided Rockets," Pergamon Press 1964, p. 94.
2. Imai, K. and Matsukawa, S., "Ballistic Equations for Spinstabilized Projectile," Memoir of N.D.A. Japan 1976, vol. 13, No. 2.
3. Imai, K. and Ogawa, K., "A FORTRAN Program for Calculation of the Firing Table of Guns," Memoir of N.D.A. Japan 1980, vol. 17, No. 3.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Tehcnical Information Center Cameron Station Alexandria, Virginia 22314	2
2. Library, Code 0142 Naval Postgraduate School Monterey, California 93940	2
3. Chairman, Code 67 Department of Aeronautics Naval Postgraduate School Monterey, California 93940	1
4. Distinguished Professor A. E. Fuhs Code 67Fu Department of Aeronautics Naval Postgraduate School Monterey, California 93940	4
5. LTC Rene Larriva, USMC Defense Advanced Research Projects Agency 1400 Wilson Blvd. Arlington, Virginia 22209	2
6. Commander, Naval Sea Systems Command Naval Sea Systems Command Headquarters Attn: Code 62YC Washington, D.C. 20362	1
7. Commander, U.S. Army Armament Research and Development Command (ARRAD COM) Attn: Mr. Lou Marino Dover, NJ 07801	1
8. Deputy Chief of Staff for Research, Development and Studies Headquarters USMC Washington, D.C. 20370	1
9. Commander Development Command USMC Base Quantico, Virginia 22134	1
10. Commander Artillery Development Command Fort Sill, Oklahoma 73503	1

11. Mr. Art Thomas
Vice President, Engineering
The Marquardt Company
16555 Saticoy Street
Van Nuys, California 91409

1

12. Mr. Joseph G. Bendot
The Marquardt Company
16555 Saticoy Street
Van Nuys, California 91409

1

13. Dr. Odad Amichai
Visiting Research Associate
Department of Aeronautics
Naval Postgraduate School
Monterey, California 93940

4